1N5817 and 1N5819 are Preferred Devices

# **Axial Lead Rectifiers**

This series employs the Schottky Barrier principle in a large area metal-to-silicon power diode. State-of-the-art geometry features chrome barrier metal, epitaxial construction with oxide passivation and metal overlap contact. Ideally suited for use as rectifiers in low-voltage, high-frequency inverters, free wheeling diodes, and polarity protection diodes.

## **Features**

- $\bullet$  Extremely Low V<sub>F</sub>
- Low Stored Charge, Majority Carrier Conduction
- Low Power Loss/High Efficiency
- These are Pb-Free Devices\*

## **Mechanical Characteristics:**

- Case: Epoxy, Molded
- Weight: 0.4 Gram (Approximately)
- Finish: All External Surfaces Corrosion Resistant and Terminal Leads are Readily Solderable
- Lead Temperature for Soldering Purposes: 260°C Max for 10 Seconds
- Polarity: Cathode Indicated by Polarity Band
- ESD Ratings: Machine Model =  $C$  (>400 V) Human Body Model =  $3B$  (>8000 V)



## **ON Semiconductor®**

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## **SCHOTTKY BARRIER RECTIFIERS** 1.0 AMPERE 20, 30 and 40 VOLTS



**MARKING DIAGRAM** 



=Assembly Location A 1N581x =Device Number x= 7, 8, or 9 YY  $=$ Year =Work Week **WW** =Pb-Free Package  $\blacksquare$ (Note: Microdot may be in either location)

### **ORDERING INFORMATION**

See detailed ordering and shipping information on page 6 of this data sheet.

Preferred devices are recommended choices for future use

\*For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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and best overall value.

### **MAXIMUM RATINGS**



Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the<br>Recommended Operating Conditions is not implied. Extended exposure to stresses above the Rec device reliability.

#### **THERMAL CHARACTERISTICS (Note 1)**



**ELECTRICAL CHARACTERISTICS** ( $T_L$  = 25°C unless otherwise noted) (Note 1)



1. Lead Temperature reference is cathode lead 1/32 in from case.<br>2. Pulse Test: Pulse Width = 300 µs, Duty Cycle = 2.0%.

 $(3)$ 

#### **NOTE 3. - DETERMINING MAXIMUM RATINGS**

Reverse power dissipation and the possibility of thermal runaway must be considered when operating this rectifier at reverse voltages above 0.1 V<sub>RWM</sub>. Proper derating may be accomplished by use of equation (1).

$$
T_{A(max)} = T_{J(max)} - R_{\theta JA}P_{F(AV)} - R_{\theta JA}P_{R(AV)}
$$
(1)  
where  $T_{A(max)} =$  Maximum allowable ambient temperature  
 $T_{J(max)} =$  Maximum allowable junction temperature  
(125°C or the temperature at which thermal  
runaway occurs, whichever is lowest)  
 $P_{F(AV)} =$  Average forward power dissipation  
 $P_{R(AV)} =$  Average reverse power dissipation  
 $R_{\theta JA} =$  Junction–to–ambient thermal resistance

Figures 1, 2, and 3 permit easier use of equation  $(1)$  by taking reverse power dissipation and thermal runaway into consideration. The figures solve for a reference temperature as determined by equation (2).

$$
T_R = T_{J(max)} - R_{\theta JA} P_{R(AV)} \tag{2}
$$

Substituting equation (2) into equation (1) yields:

$$
T_{A(max)} = T_R - R_{0,IA} P_{F(AV)}
$$

Inspection of equations (2) and (3) reveals that  $T_R$  is the ambient temperature at which thermal runaway occurs or where  $T_J = 125^{\circ}C$ , when forward power is zero. The transition from one boundary condition to the other is evident on the curves of Figures 1, 2, and 3 as a difference in the rate of change of the slope in the vicinity of  $115^{\circ}$ C. The data of Figures 1, 2, and 3 is based upon dc conditions. For use in common rectifier circuits, Table 1 indicates suggested factors for an equivalent dc voltage to use for conservative design, that is:

$$
V_{R(\text{equiv})} = V_{\text{in(PK)}} \times F \tag{4}
$$

The factor F is derived by considering the properties of the various rectifier circuits and the reverse characteristics of Schottky diodes.

EXAMPLE: Find  $T_{A(max)}$  for 1N5818 operated in a 12-volt dc supply using a bridge circuit with capacitive filter such that  $I_{DC} = 0.4$  A ( $I_{F(AV)} = 0.5$  A),  $I_{(FM)}/I_{(AV)} = 10$ , Input Voltage = 10  $V$ <sub>(rms)</sub>,  $R_{\theta JA}$  = 80°C/W.

Step 1. Find  $V_{R(equiv)}$ . Read F = 0.65 from Table 1,  $\therefore$  V<sub>R(equiv)</sub> = (1.41)(10)(0.65) = 9.2 V. Step 2. Find T<sub>R</sub> from Figure 2. Read T<sub>R</sub> = 109°C  $\overset{\sim}{\omega}$  V<sub>R</sub> = 9.2 V and R<sub>θJA</sub> = 80°C/W.<br>Step 3. Find P<sub>F(AV)</sub> from Figure 4. \*\*Read P<sub>F(AV)</sub> = 0.5 W  $\frac{I_{(FM)}}{I_{(AV)}}$  = 10 and IF(AV) = 0.5 A.

\*\*Values given are for the 1N5818. Power is slightly lower for the 1N5817 because of its lower forward voltage, and higher for the 1N5819.







\*\*Note that  $V_{R(PK)} \approx 2.0 V_{in(PK)}$ .

 $\dagger$ Use line to center tap voltage for  $V_{\text{in}}$ 





**Figure 5. Forward Power Dissipation** 1N5817-19





#### **NOTE 4. - MOUNTING DATA**

Data shown for thermal resistance, junction-to-ambient  $(R<sub>HJA</sub>)$  for the mountings shown is to be used as typical guideline values for preliminary engineering, or in case the tie point temperature cannot be measured.

TYPICAL VALUES FOR  $R_{\theta$ JA IN STILL AIR

<b>Mounting</b>	Lead Length, L (in)				
Method	1/8	1/4	1/2	3/4	$R_{\theta$ JA
	52	65	72	85	$\degree$ C/W
	67	80	87	100	$\degree$ C/W
	50				°C/W

**Mounting Method 1** 

P.C. Board with  $1 - 1/2'' \times 1 - 1/2''$ copper surface.





P.C. Board with  $1 - 1/2'' \times 1 - 1/2''$ copper surface.





nting Method 2

€

**VECTOR PIN MOUNTING** 

#### **NOTE 5. - THERMAL CIRCUIT MODEL**

(For heat conduction through the leads)



Use of the above model permits junction to lead thermal resistance for any mounting configuration to be found. For a given total lead length, lowest values occur when one side of the rectifier is brought as close as possible to the heatsink. Terms in the model signify:

 $T_C$  = Case Temperature

 $T_A$  = Ambient Temperature

(Subscripts A and K refer to anode and cathode sides, respectively.) Values for thermal resistance components are:  $R_{\theta I}$  = 100°C/W/in typically and 120°C/W/in maximum  $R_{\theta J}$  = 36°C/W typically and 46°C/W maximum.



#### **NOTE 6. - HIGH FREQUENCY OPERATION**

Since current flow in a Schottky rectifier is the result of majority carrier conduction, it is not subject to junction diode forward and reverse recovery transients due to minority carrier injection and stored charge. Satisfactory circuit analysis work may be performed by using a model consisting of an ideal diode in parallel with a variable capacitance. (See Figure 10.)

Rectification efficiency measurements show that operation will be satisfactory up to several megahertz. For example, relative waveform rectification efficiency is approximately 70 percent at 2.0 MHz, e.g., the ratio of dc power to RMS power in the load is 0.28 at this frequency, whereas perfect rectification would yield 0.406 for sine wave inputs. However, in contrast to ordinary junction diodes, the loss in waveform efficiency is not indicative of power loss: it is simply a result of reverse current flow through the diode capacitance, which lowers the dc output voltage.



**Figure 10. Typical Capacitance** 

#### **ORDERING INFORMATION**



†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

\*This package is inherently Pb-Free.







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Europe, Middle East and Africa Technical Support: Phone: 00421 33 790 2910 For additional information, please contact your local Sales Representative